- $C_{max}$ = $C_{min}$ +0.3+(%Cr-12)×0.06, balance iron including incidental impurities, the powder being formed by rapid atomisation followed by an annealing treatment such that the powder contains at least 12% of chromium in solution and a dispersion of carbides.
- 3. An alloy powder according to claim 2 having a stable substantially fully ferritic matrix.
- **4.** An article produced from an alloy powder according to claim **1**, formed by a powder metallurgy process comprising forming a shape from the powder by compaction followed 10 by sintering without the application of external pressure.
- 5. The article of claim 4, wherein said alloy powder is mixed with a conventional stainless steel powder.
- **6**. An article produced from an alloy powder according to claim **2**, formed by a powder metallurgy process comprising 15 forming a shape from the powder by compaction followed by sintering without the application of external pressure.
- 7. The article of claim 6, wherein said alloy powder is mixed with a conventional stainless steel powder.
- 8. A method of producing articles by a powder metallurgy 20 process comprising forming a shape by compaction of a powder followed by sintering without the application of external pressure or deformation, in which the powder is a stainless steel alloy powder which has been produced by rapid atomisation followed by an annealing treatment, the 25 alloy powder comprising, in weight percent, chromium 14 to 30, molybdenum 1 to 5, vanadium 0 to 5, tungsten 0 to 6, silicon 0 to 1.5, carbon according to the formula set forth below, a strong carbide forming element 0 to 5, wherein the total of Mo, V and W being at least 3, the balance being iron 30 including incidental impurities, the alloy powder together with any addition of free graphite powder mixed therewith having a minimum and maximum carbon content according to  $C_{min}$ =(%V×0.24)+(2×%Mo+%W)×0.03+(%Nb×0. 13)+  $(\%\text{Ti}\times0.25)+(\%\text{Ta}\times0.066)$ , and
  - C<sub>max</sub>=C<sub>min</sub>+0.3+(%Cr-12)×0.06, such that the powder has a sufficient carbon content to form carbides with all

- the Mo, V, W and other strong carbide forming elements present while leaving at least 12% chromium in solution in the matrix.
- 9. A method according to claim 8, further comprising the
  5 steps of sintering the article in the range 1050° C. to 1350° C. for a period of 10 minutes to three hours, and cooling the article at a rate in the range 10° C. to 200° C. per minute.
  - 10. A method according to claim 8, further comprising the step of mixing the alloy powder with an additional free graphite powder.
  - 11. A method according to claim 8, in which the annealing treatment comprises annealing under vacuum for 12 to 100 hours at a temperature in the range 700° C. to 1050° C.
  - 12. An article produced by the method of claim 8, comprising an article consisting of a distribution of carbides embedded in a substantially ferritic matrix containing at least 12% by weight of chromium in solution, said article being free of the necessity for further heat treatment.
  - 13. Articles according to claim 12, in which the alloy powder comprises, in weight percent, chromium 20 to 28, molybdenum 2 to 3, vanadium 1.5 to 2.5, tungsten 2.5 to 3.5, silicon 08 to 1.5, carbon 0.555 to 2, a strong carbide forming element 0 to 5, and balance iron including incidental impurities.
  - 14. An alloy powder comprising, in weight percent, chromium 14 to 30, molybdenum 1 to 5, vanadium 0 to 5, tungsten 0 to 6, silicon 0 to 1.5, carbon  $C_{min}$  to  $C_{max}$ , a strong carbide forming element 0 to 5, and a balance iron including incidental impurities,
    - wherein  $C_{min}$ =(%V×0.24)+(2×%Mo+%W)×0.03+(%Nb× 0.13)+(%Ti×0.25)+(%Ta×0.066) and  $C_{max}$ = $C_{min}$ +0.3+ (%Cr-12)×0.06, such that the powder includes sufficient carbon to form carbides with all the Mo, V, W and strong carbide forming element present in the powder.

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